

Use of Analytical Models in Prospect Evaluation of Gas Hydrate Reservoirs

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Hart Conference – Commercialization of Gas Hydrates

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SCHULICH
School of Engineering

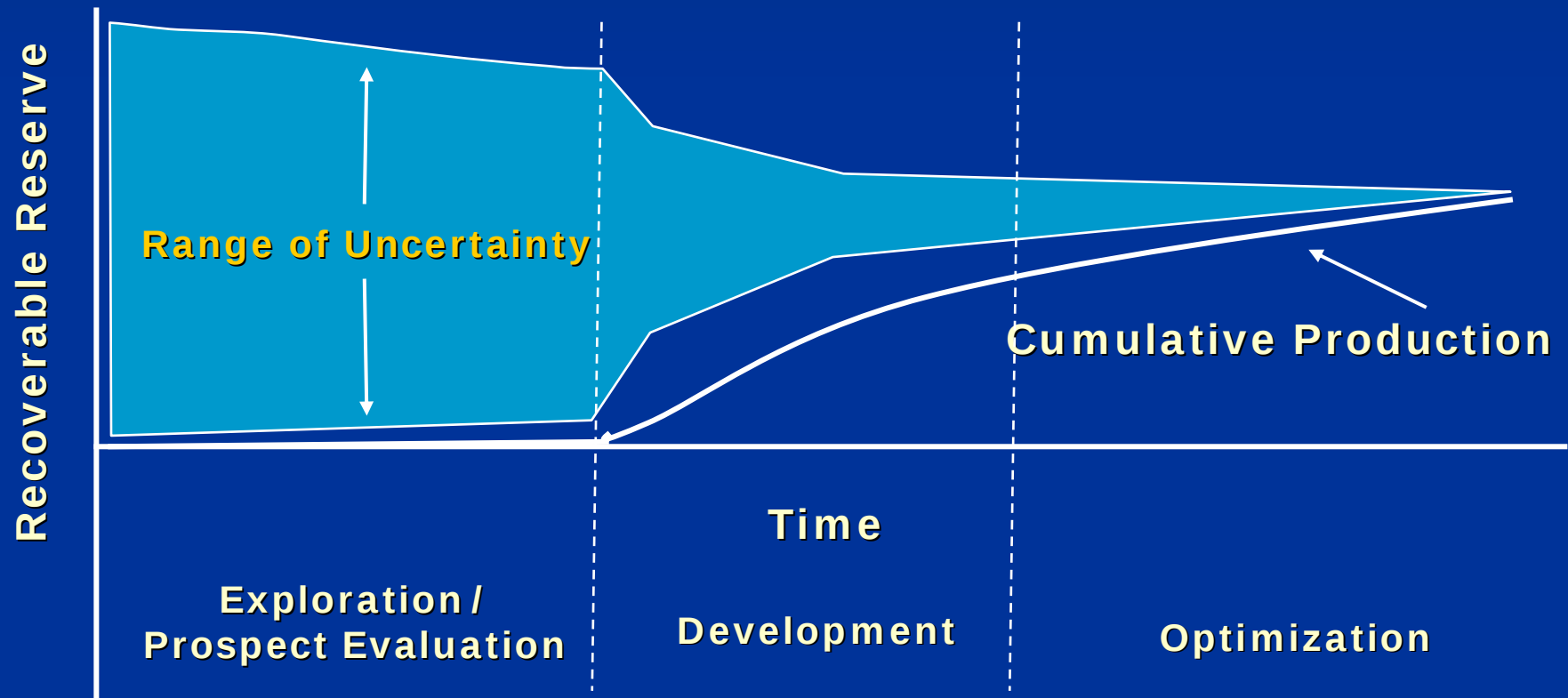


Prospect Evaluation: Realm of High Uncertainty

Limited Data

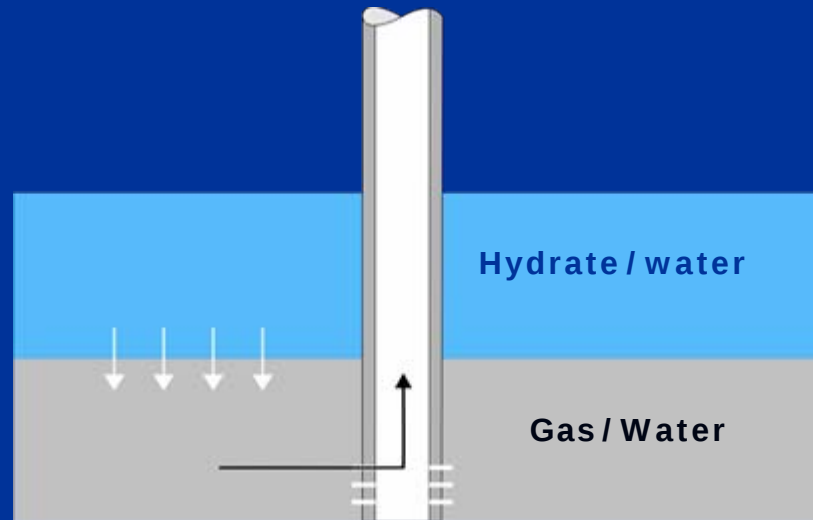
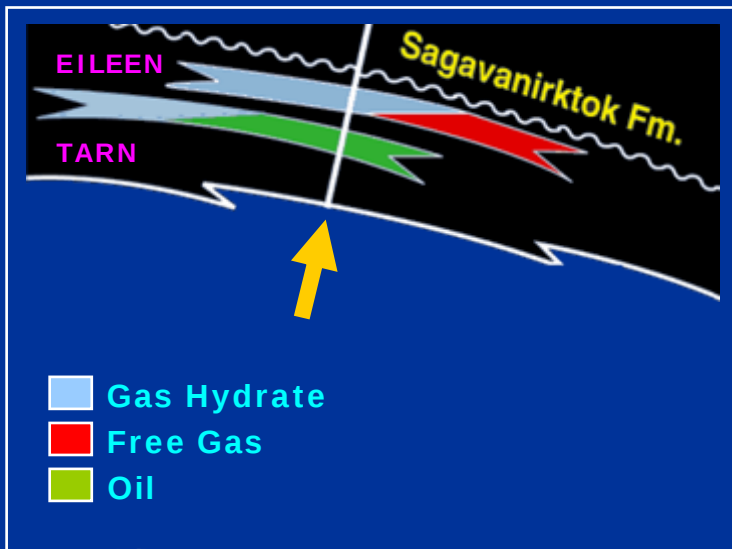
Need for large number of runs
and risk analysis

→ Analytical Models



Objectives

- For a hydrate reservoir with underlying free gas
 - Develop, validate and use analytical models for quantifying of
 - The upside in gas recovery associated with the hydrates (forward model)
 - Hydrate reserve (backward model)



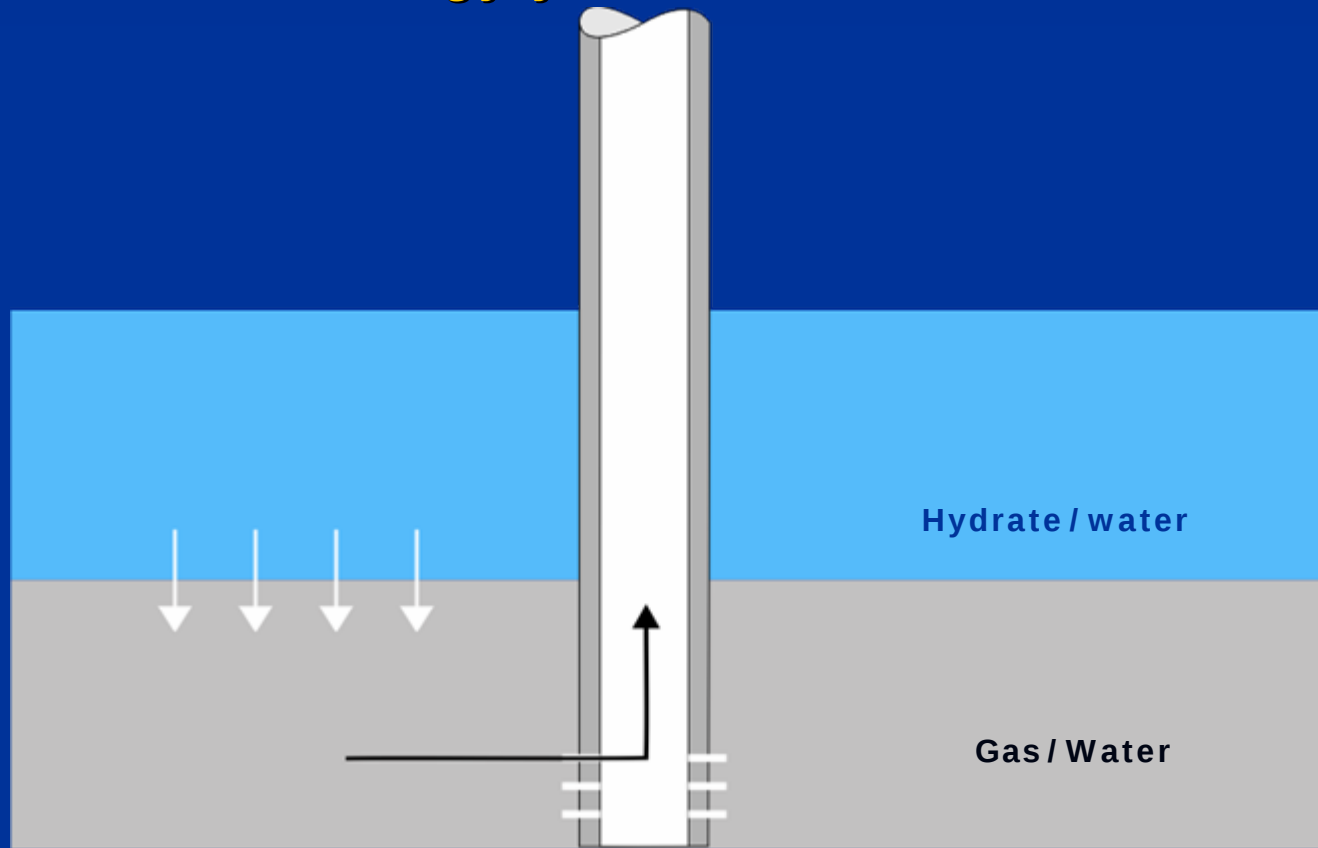
Production by Depressurization

Simplest: Produce from the gas

Least energy intensive: No external heating agent

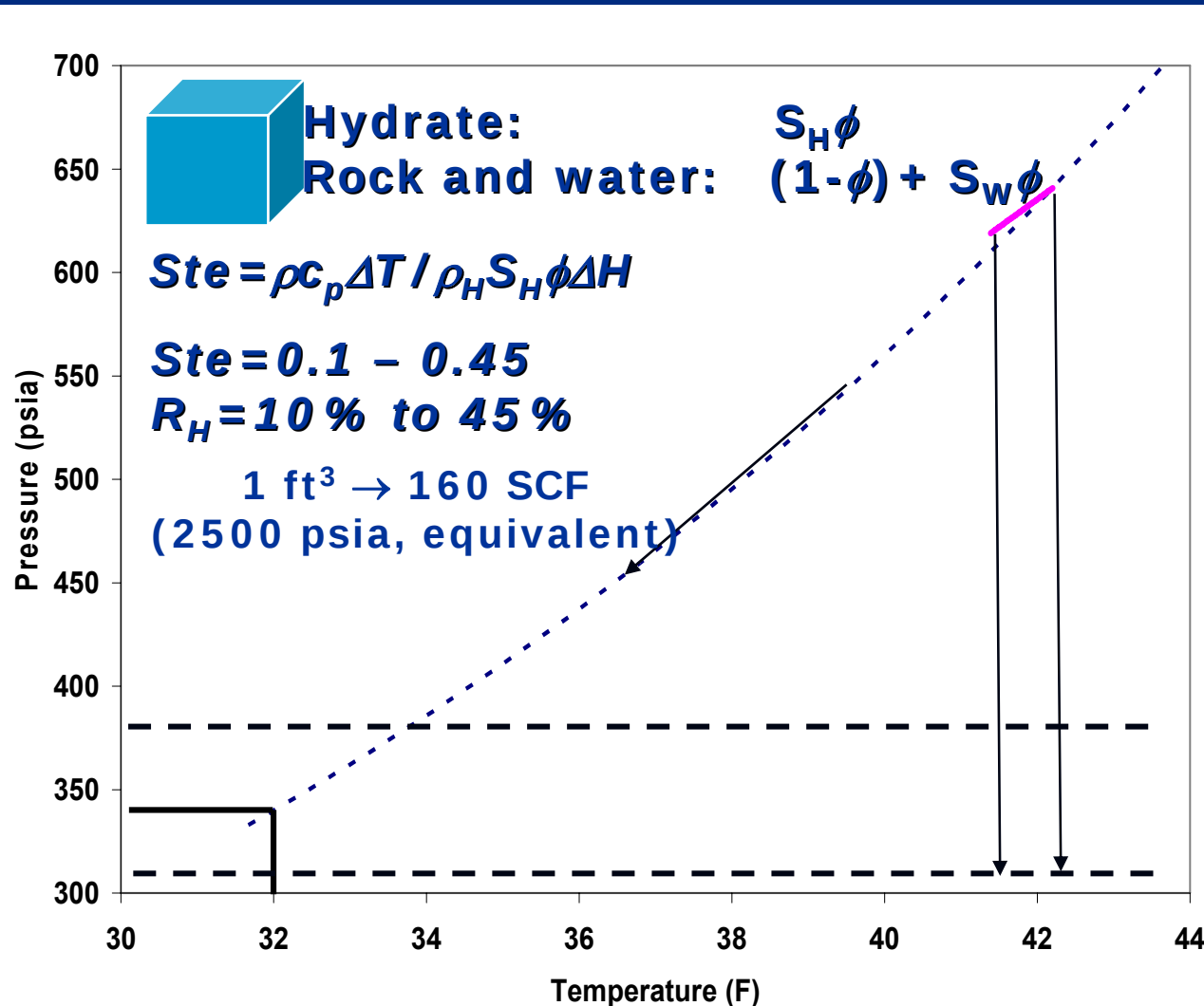
Examples: Messoyakha, Alaska, Mackenzie Delta

Not a proven technology yet: Use mathematical models!!



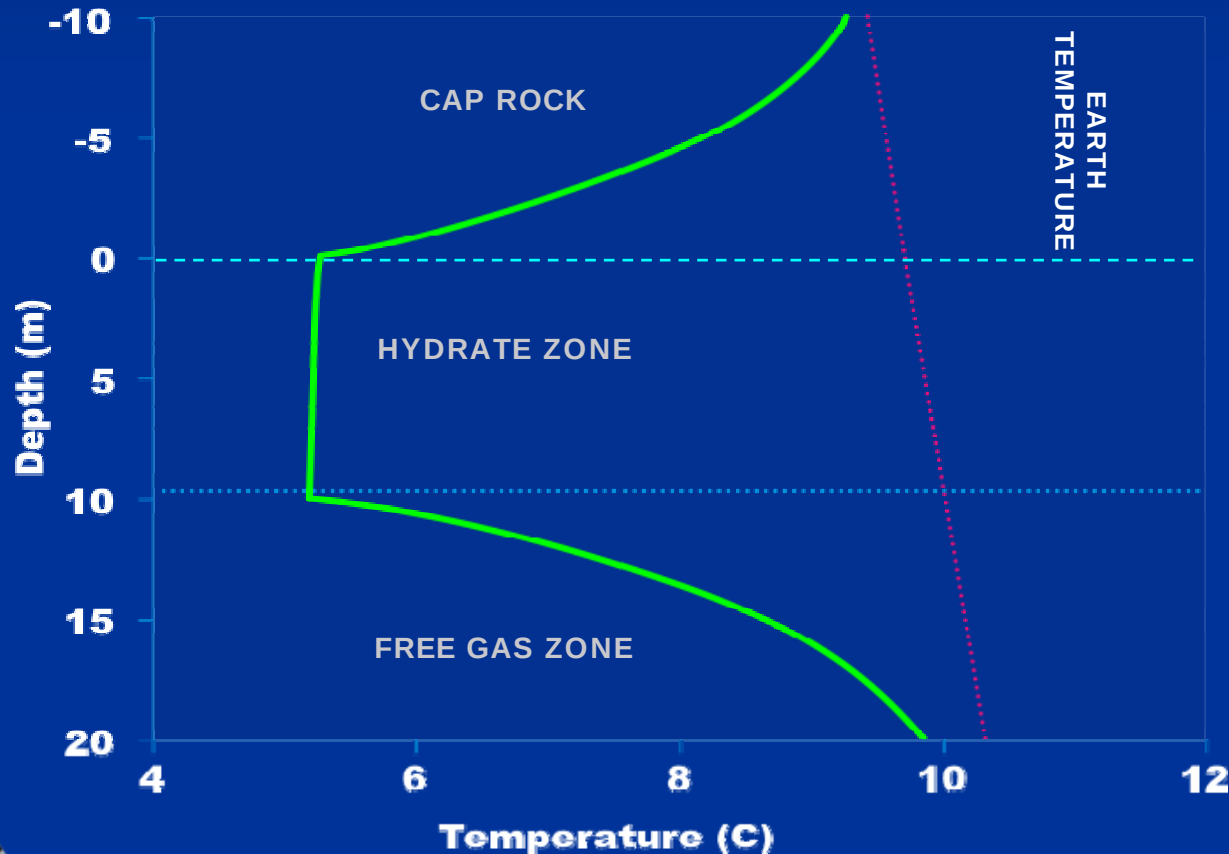
Depressurization Mechanisms

- **Decomposition rate is controlled by our ability to**
 1. Provide heat of decomposition: 11,000 BTU/ft³ hydrate



Depressurization Mechanisms

- **Decomposition rate is controlled by our ability to**
 - Provide heat of decomposition: 11,000 BTU/ft³ hydrate
 - From surrounding rock



Depressurization Mechanisms

- **Decomposition rate is controlled by our ability to**
 1. Increase the permeability of the hydrate zone
 2. Reduce the pressure within the hydrate zone

$$r_i = \sqrt{\frac{kt}{948\phi\mu c_t}}$$

$K(S_H) = 0.01 \text{ mD}$

$\phi = 30 \%$

$\mu = 1 \text{ cp}$

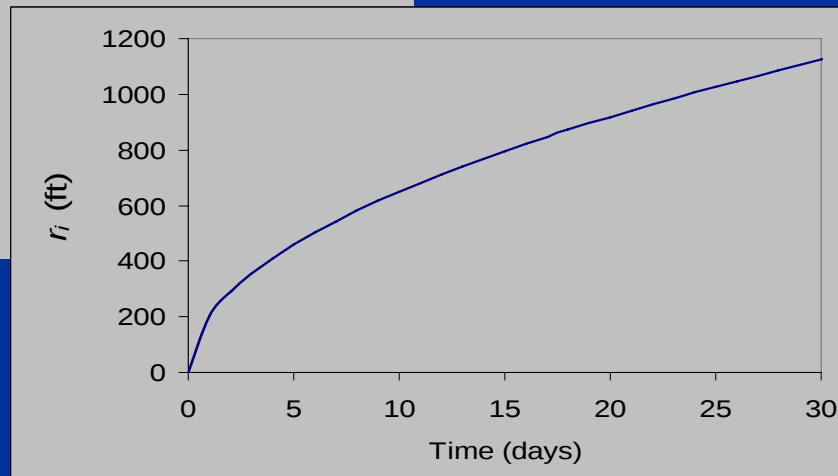
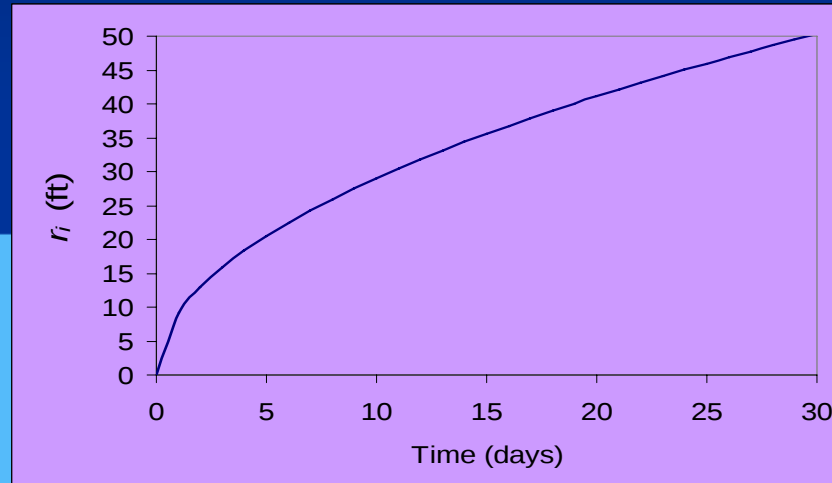
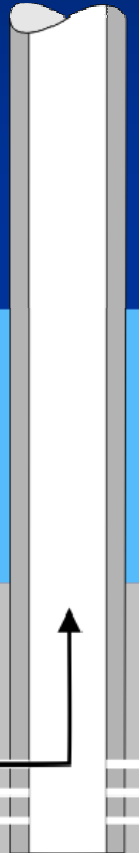
$c_t = 1 \times 10^{-5} \text{ psi}^{-1}$

$K = 10 \text{ mD}$

$\phi = 30 \%$

$\mu = 0.02 \text{ cp}$

$c_t = 1 \times 10^{-3} \text{ psi}^{-1}$



Depressurization Mechanisms

- **Decomposition rate is controlled by our ability to**
 1. Increase the permeability of the hydrate zone
 2. Reduce the pressure within the hydrate zone

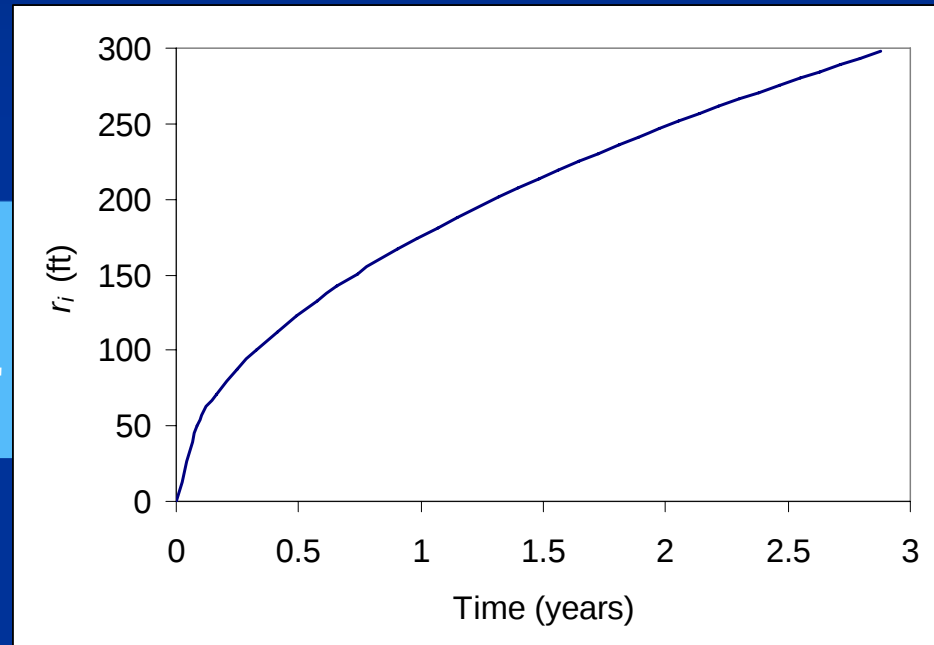
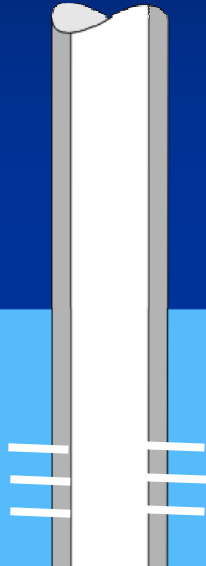
$$r_i = \sqrt{\frac{kt}{948\phi\mu c_t}}$$

$K(S_H) = 0.01 \text{ mD}$

$\phi = 30 \%$

$\mu = 1 \text{ cp}$

$c_t = 1 \times 10^{-5} \text{ psi}^{-1}$



Development of Analytical Model

■ Assumptions

- Deep decomposition
 - No vertical gradient (time-scale of one month)
- Tank-type model (zero-dimensional modeling)
 - No radial gradient (time-scale of one month)
- Equilibrium decomposition
- Complete contact between the gas and the hydrate
- No water flow
- Constant gas production rate

A Material (& Energy) Balance Equation

■ Material Balance

- $G_p = q \cdot t$
- G_H = Gas generated from the hydrates
- $G_p - G_H$ = Net gas produced

$$\frac{p}{Z} = \frac{p_i}{Z_i} \left(1 - \frac{G_p - G_H}{G} \right)$$

■ Heat equation:

Heat from cap and base + sensible heat =
Heat available for decomposition (G_H)

■ Equilibrium relation

$$p = \exp \left(a + \frac{c}{T} \right)$$

- The three unknowns, p , T , and G_H are found

Solutions (CIPC 2006-018)

$$q_s(t) = \frac{B_H A H \rho c_p}{\rho_H \Delta H} b(t) \left(\frac{4 \rho_r c_{pr}}{\sqrt{\pi} \rho c_p} \frac{\sqrt{\alpha_r}}{H} \sqrt{t} + 1 \right)$$

$$b(t) = \frac{q_p}{\left[\frac{1 - (p_{oe} Z_i)/(p_i Z_{oe})}{T_i - T_{oe}} G_f + \frac{B_H A H \rho c_p}{\rho_H \Delta H} \left(\frac{8}{3 H \rho c_p \sqrt{\pi}} \sqrt{k_{cr} \rho_r C_{pr} t} + 1 \right) \right]}$$

$$p = \exp\left(a + \frac{c}{T}\right)$$

$$T = T_i - b(t) t$$

Solutions (SPE 102234)

$$\psi_{wf} = \bar{\psi} - \frac{q_w p_{sc} T}{\pi T_{sc} k h_t} \left[\ln \left(\frac{r_e}{r_w} \right) - \frac{3}{4} + S \right]$$

$$Ste = \frac{\rho c_p \Delta T}{\rho_H \phi S_H \Delta H} \quad N_p = \frac{q_p / G_f}{\alpha / H^2} \quad N_b = \frac{b / \Delta T}{\alpha / H^2}$$

Validation against Numerical Simulator (Hydrsim)

■ Heat flow

- Conduction and convection
- Decomposition heat of hydrate
- Heat input from the cap / base rock
- Heat output by the producing fluids

■ Fluid flow

- Multi-phase flow through porous media
- Generation of fluids due to decomposition
- Gravity, capillary and viscous forces

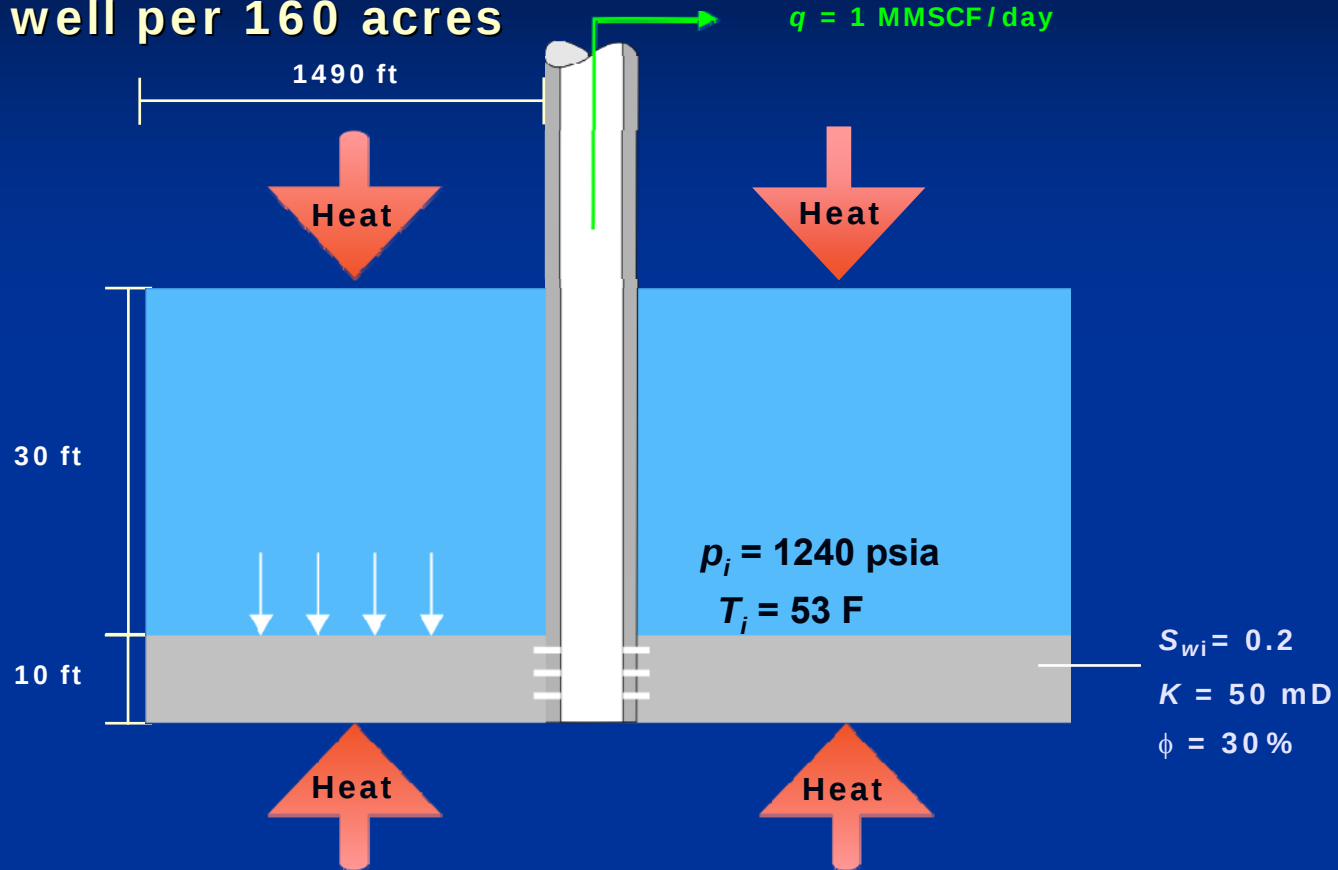
■ Intrinsic Kinetics of decomposition

- The Kim-Bishnoi model

■ No geomechanical changes

Base Case

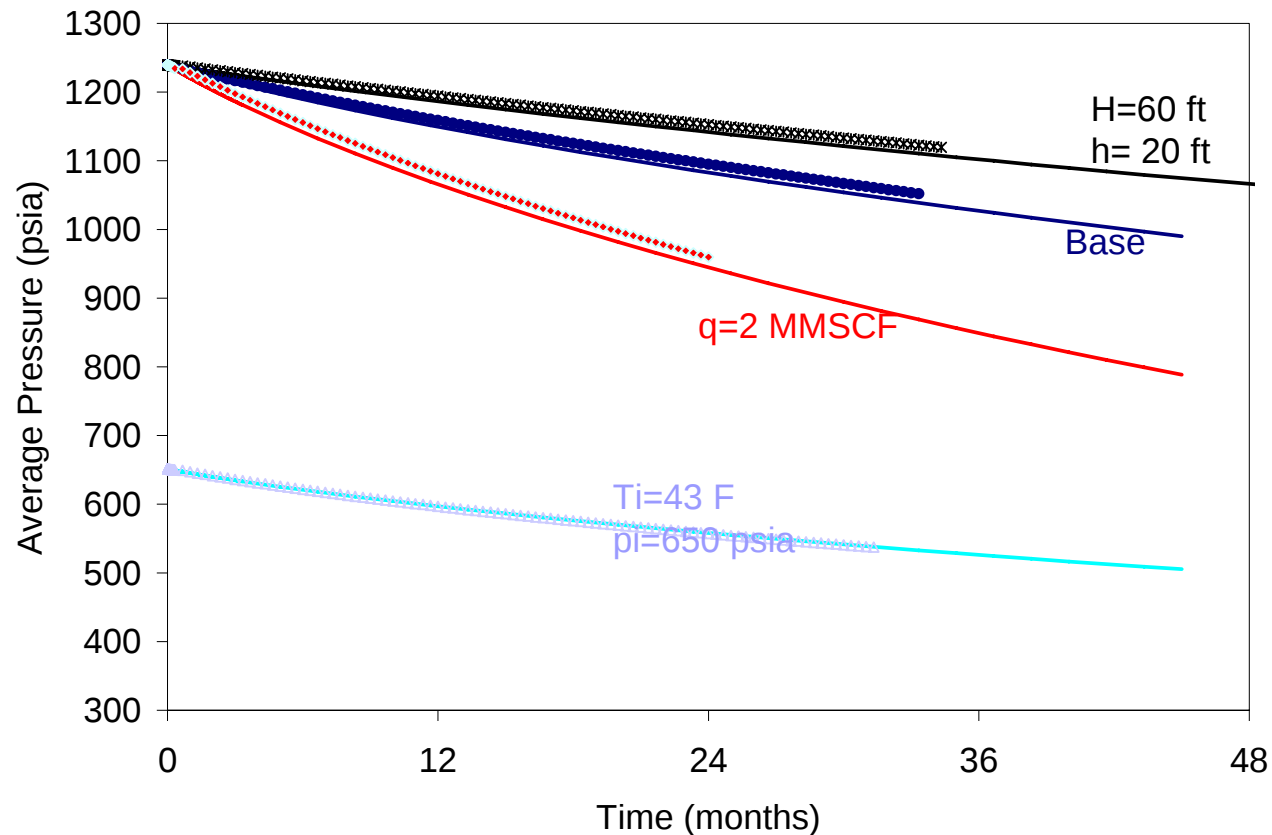
One well per 160 acres



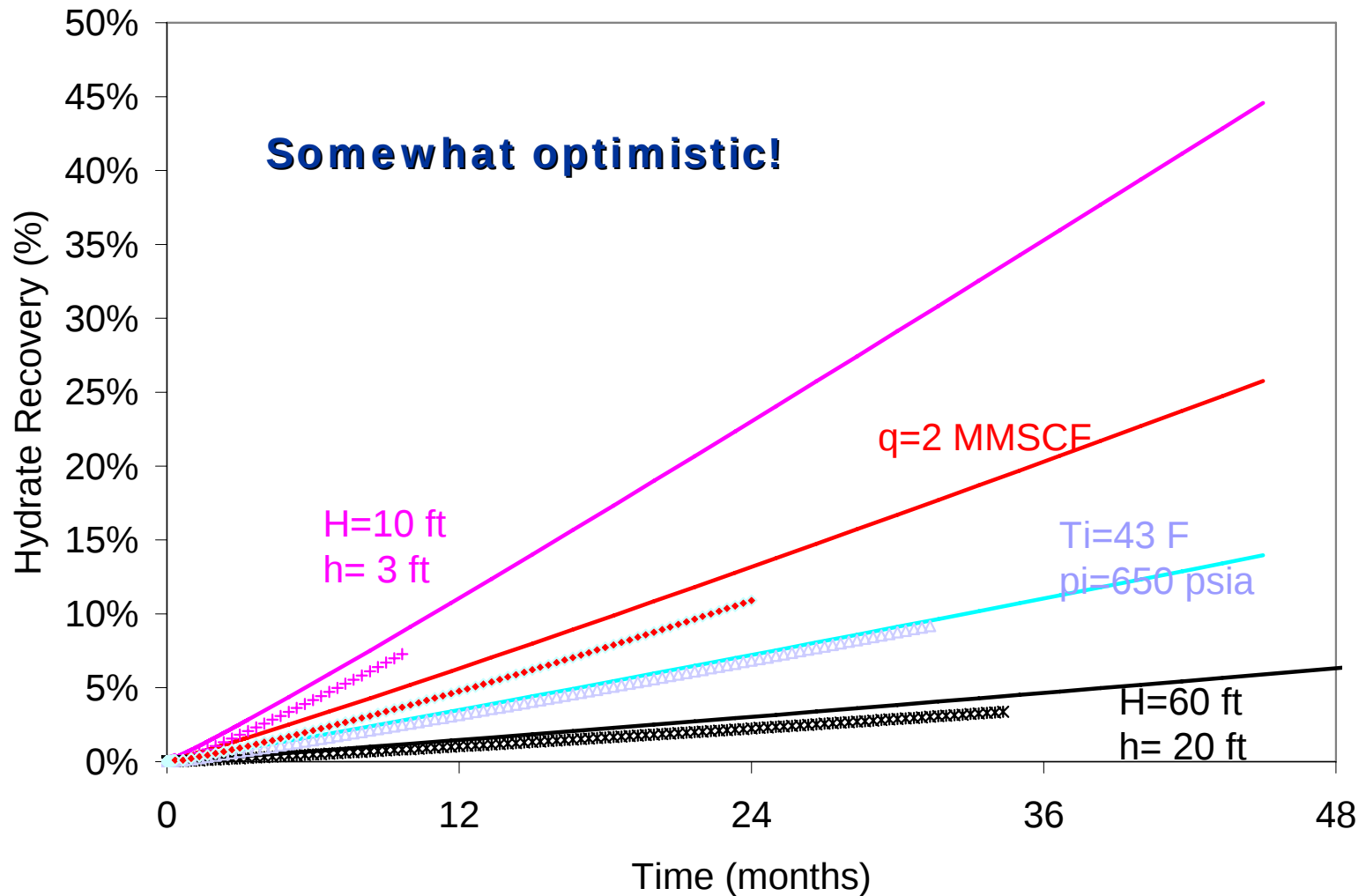
Validation – Average Pressure

■ Various Cases

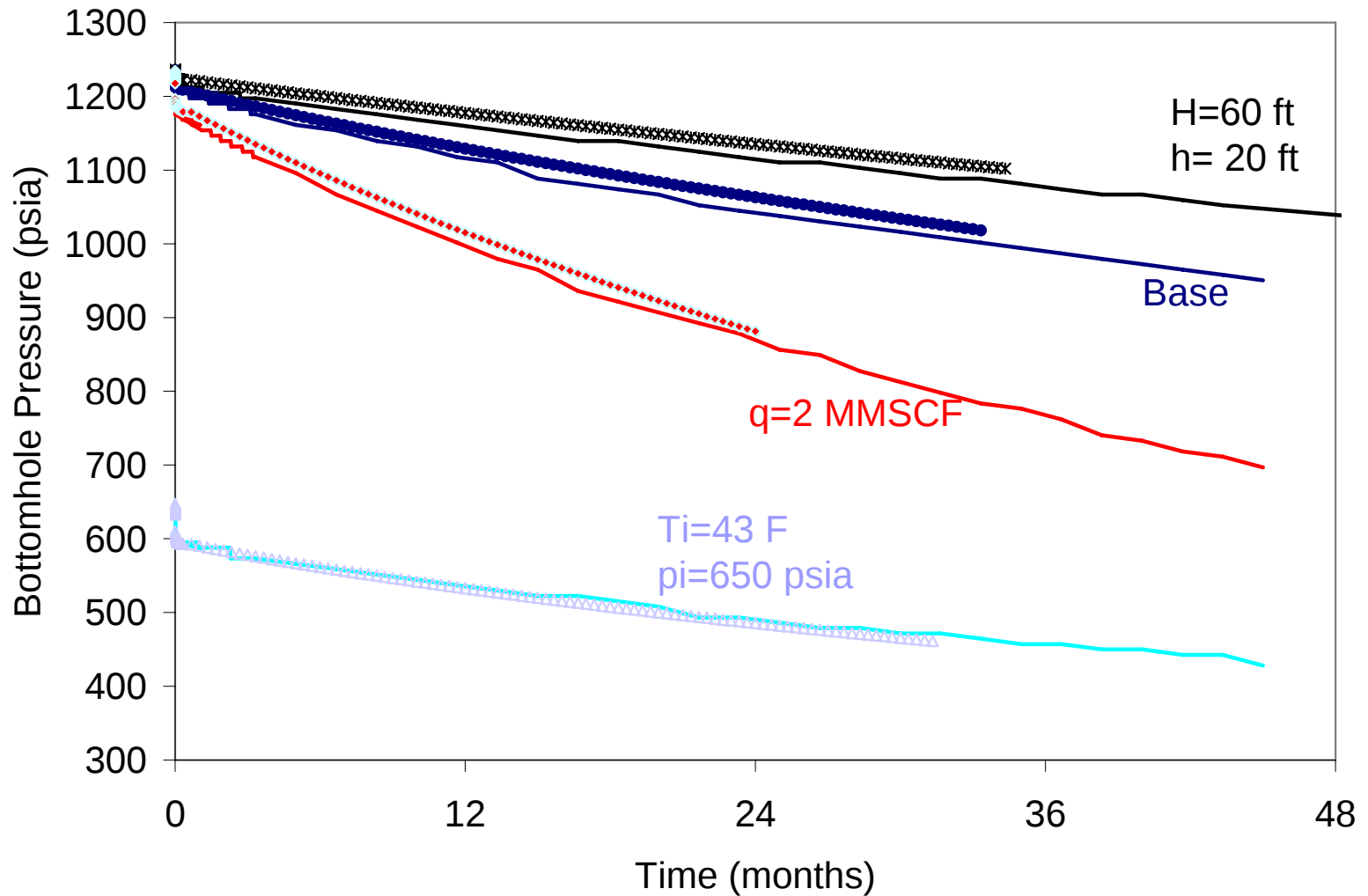
- Porosity
- Thermal conductivity
- Production rate
- Net pay
- Drainage area
- Initial Pressure
- Permeability



Validation – Hydrate Recovery



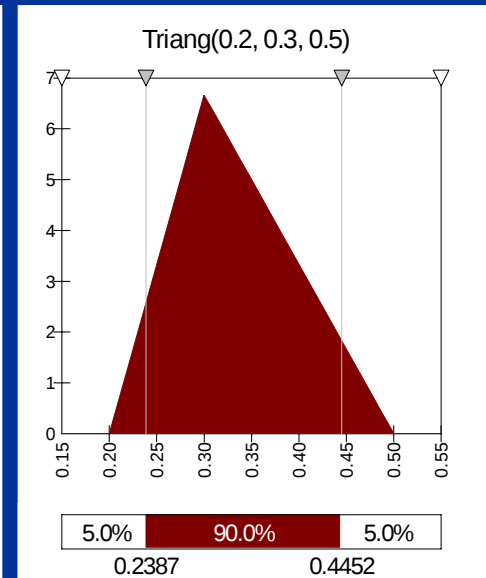
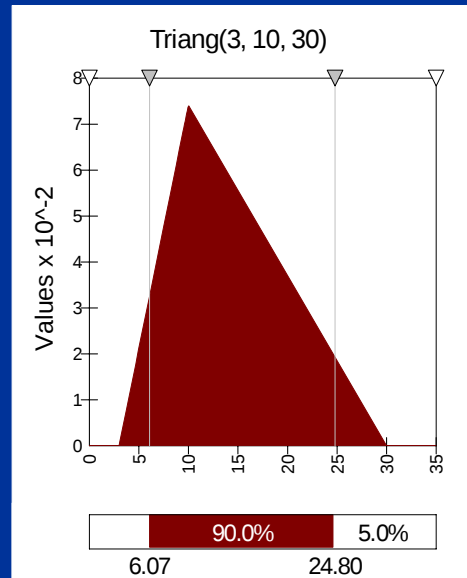
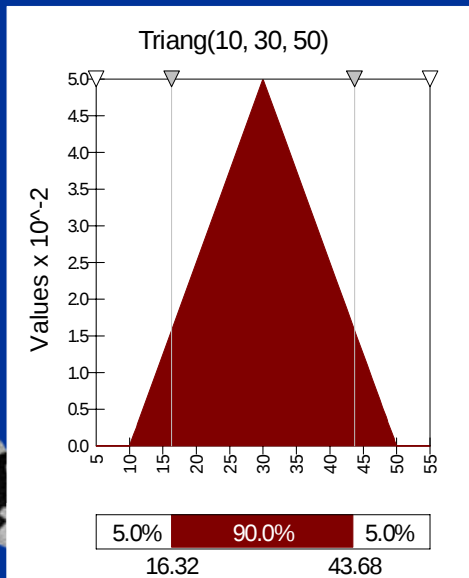
Validation – Flowing BHP



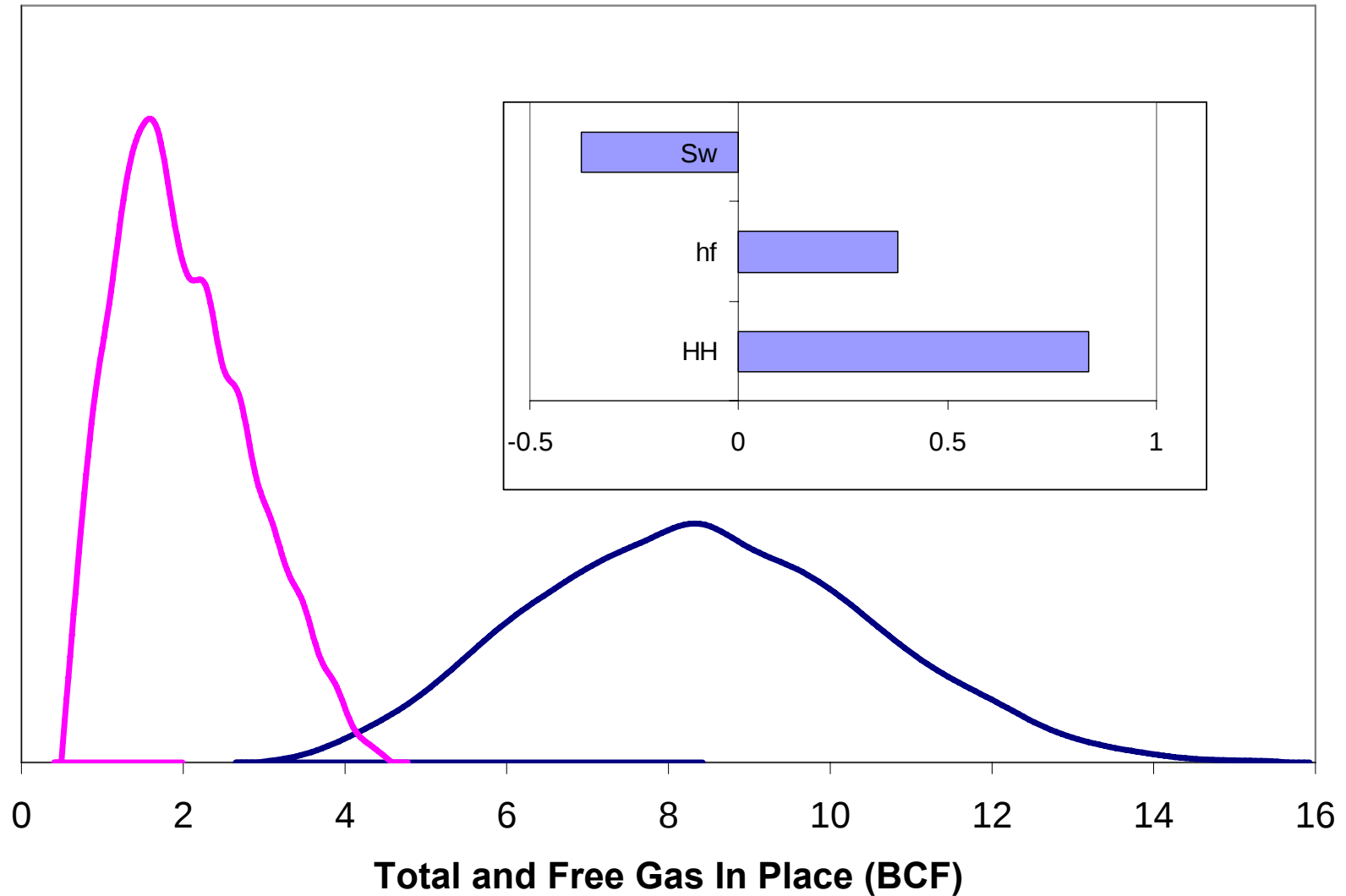
Prospect Evaluation

Uncertain Input Parameters

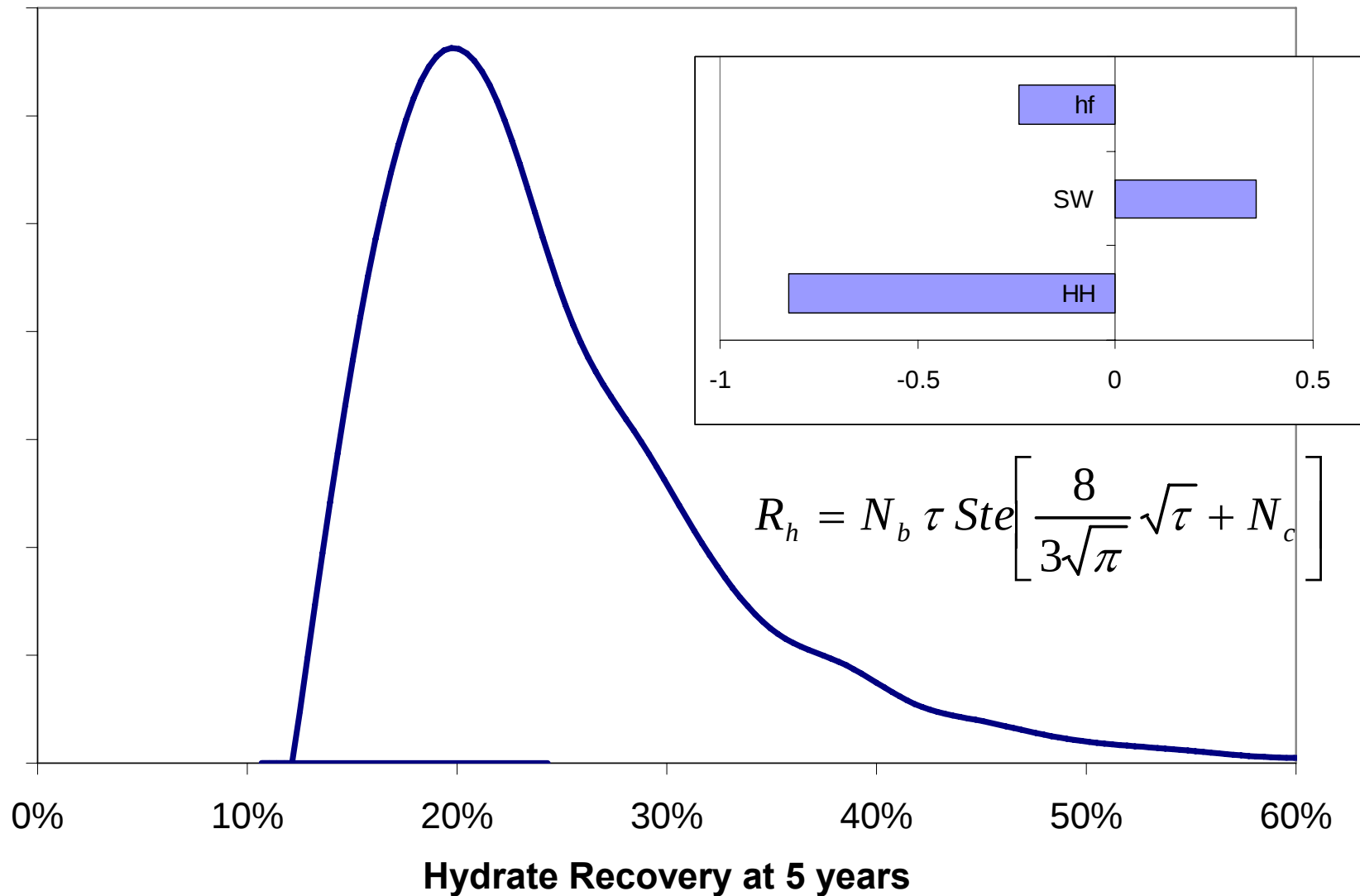
- Thickness of the hydrate layer (10, 30, 50 ft)
- Thickness of the free gas zone (3, 10, 30 ft)
- Hydrate Saturation (0.5, 0.6, 0.8)
- Porosity
- Drainage Area
- Equilibrium relation



Total vs. Free Gas In Place



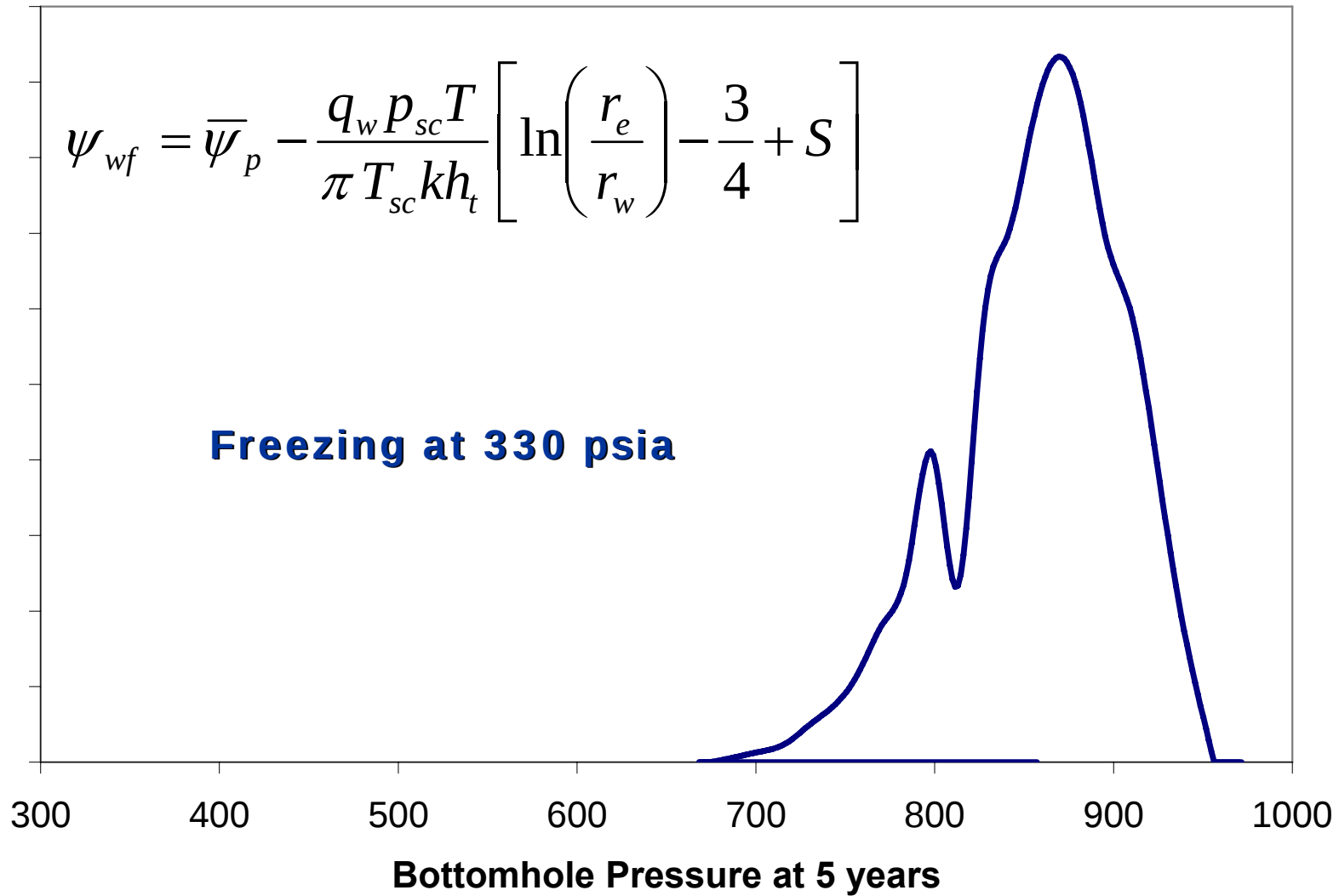
Hydrate Recovery



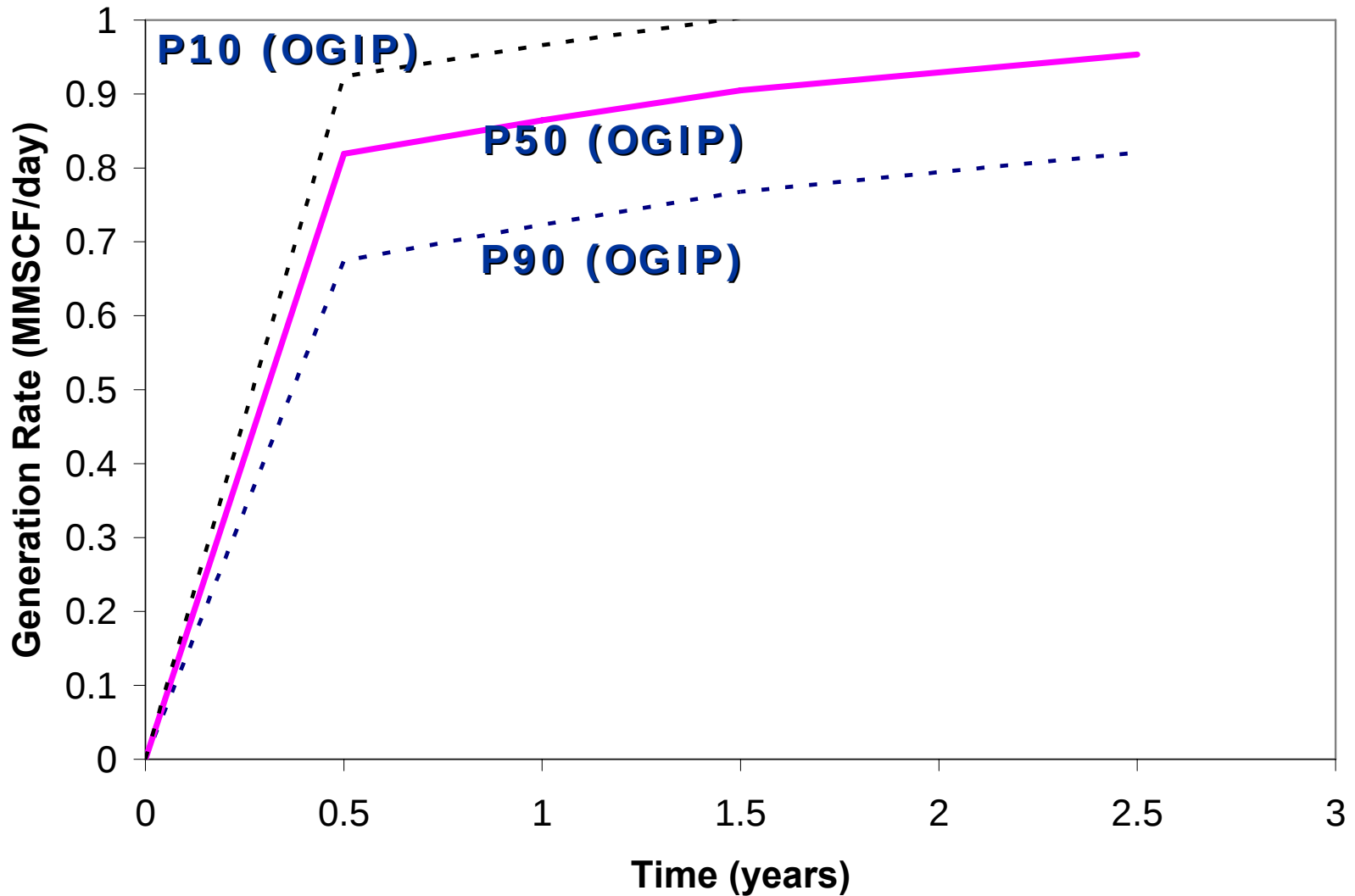
Bottomhole Pressure

$$\psi_{wf} = \bar{\psi}_p - \frac{q_w p_{sc} T}{\pi T_{sc} k h_t} \left[\ln \left(\frac{r_e}{r_w} \right) - \frac{3}{4} + S \right]$$

Freezing at 330 psia



Hydrate Contribution in Rate



Why Analytical?

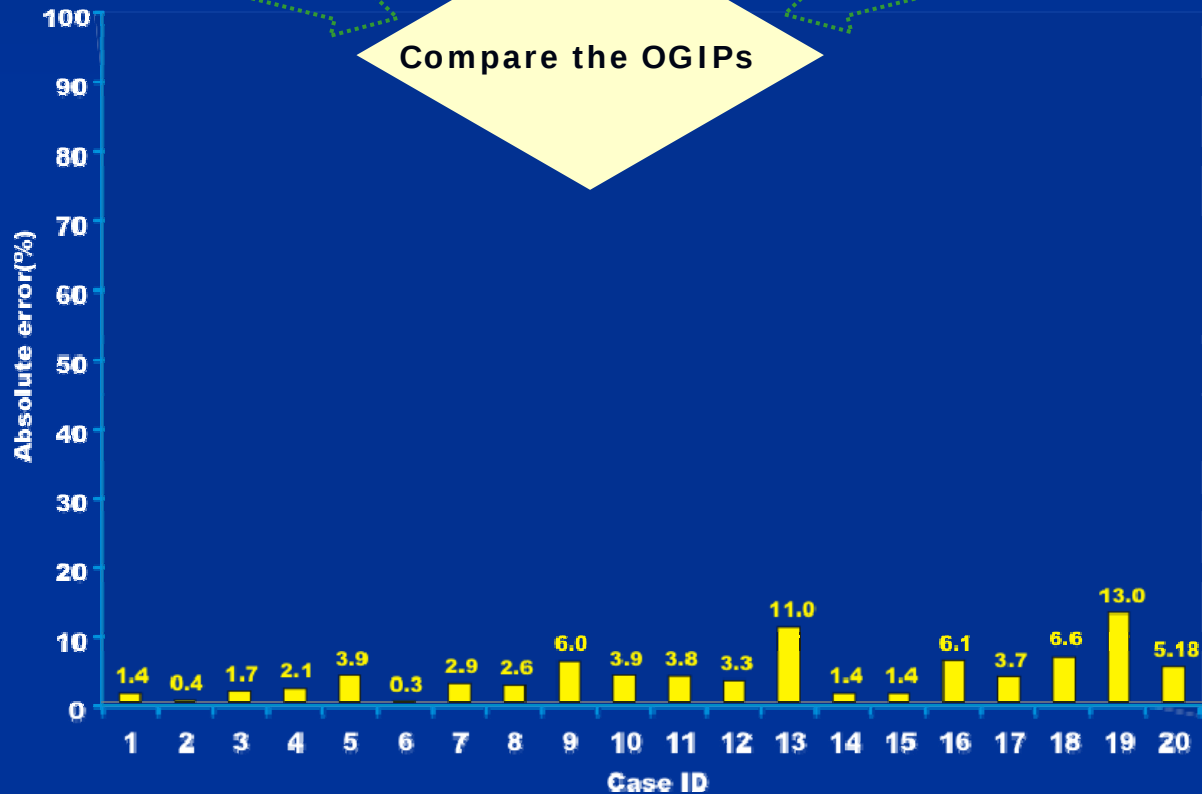
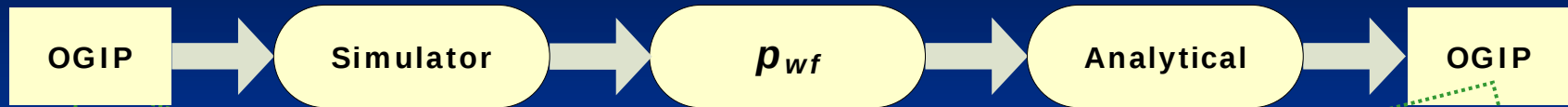
- Limited data requires risk analysis (hundred's of runs)

- Speed-up factor

- One simulation run: 10 hours
- 10,000 analytical runs: 2 minutes
- Speed-up factor: 3×10^6

- Availability and ease of use

Reserve Estimation



Conclusions

- **For the cases studied**
 - Hydrate contribution to gas production was significant
- **A “simple” material (and energy) balance equation was developed**
- **The simple model allows prospect evaluation and large number of runs required in risk analysis**
 - Evaluate the upside due to contribution of hydrates
 - Etc.
- **In an inverse mode, the model can be used for reserve estimation**

Acknowledgments

- H. Hong, S. Gerami, A. Shahbazi, ...
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- Fekete Associates Inc and Mineral Management Services
- Imperial Oil, CMG, GSC, NSERC, AERI, NRCan
- Mallik Research team, Drs. Scott Dallimore & Fred Wright

Thank you!

Questions?